TFE4120 Electromagnetism: crash course

Intensive course: Two-weeks

Lecturer: Shunguo Wang, shunguo.wang@ntnu.no

Assistant: Sandra Yuste Munoz, Sandra.y.munoz@ntnu.no

Participants: should have Bsc in electronic, electrical/ power engineering, etc.

Aim of the course: Give students a minimum pre-requisite to follow a 2-year master program in electronics or electrical/power engineering.

Information is posted there:

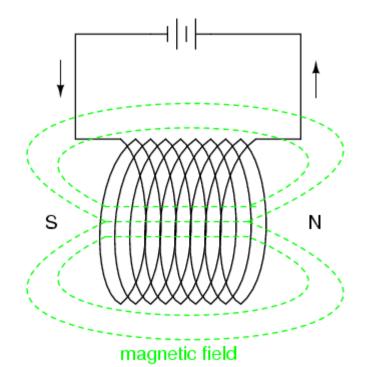
https://www.ntnu.no/wiki/display/tfe4120/Crash+Course+in+Electromagnetism+2023

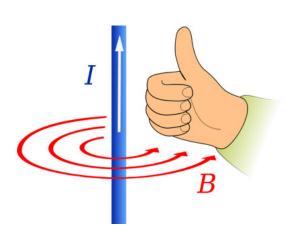
Content for lectures

- Lecture 1: Introduction and vector calculus
- Lecture 2: Electro-statics
- Lecture 3: Electro-statics
- Lecture 4: Magneto-statics
- Lecture 5: Electro-dynamics
- Lecture 6: Electro-magnetics

Lecture 1: Electro-magnetism introduction and vector calculus

- 1) What does electro-magnetism describe?
- 2) Brief induction about Maxwell equations
- 3) Electric force: Coulomb's law
- 4) Vector calculus



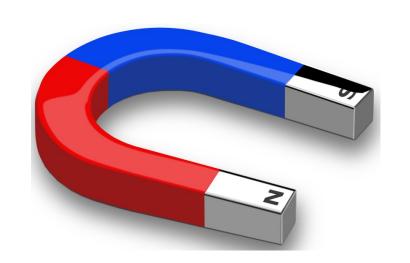


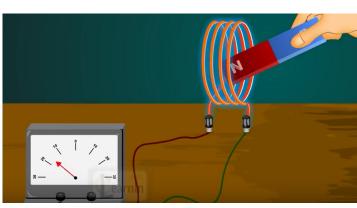
Electro-magnetism

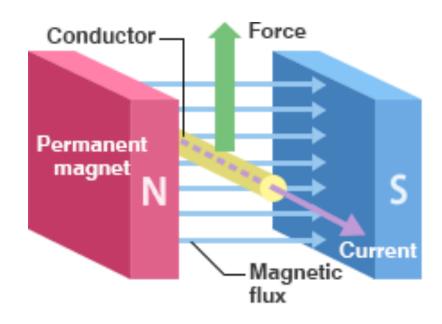
Originally, electricity and magnetism were considered to be two separate phenomena.

Electro-magnetism: Physical interaction between electricity and magnetism.

Electromagnetic force: One of the four fundamental interactions in the nature (gravitation, electromagnetism, the strong and weak forces).







History

Carl Friedrich Gauss (1777-1855): German mathematician and physicist

The electric flux out of a closed surface = total enclosed charge divided by the permittivity of free space

Electrostatics

$$\nabla \cdot \mathbf{E} = \frac{\rho}{\varepsilon_0}$$

$$\nabla \cdot \mathbf{H} = 0$$

Andre-Marie Ampere (1775-1836): French physicist and mathematician

The magnetic field produced by an electric current is proportional to the magnitude of the current times a constant equal to the permeability of free space (μ_0)

Magnetostatics

$$\nabla \times \mathbf{B} = \mu_0 \mathbf{J}$$

Michael Faraday (1791-1867): English Scientist

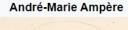
In 1831 Faraday observed that a moving magnet could induce a current in a circuit and a changing current could, through its magnetic effects, induce a current to flow in another circuit.

Magneto-dynamics

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

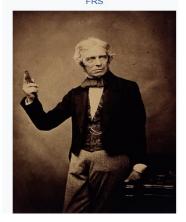


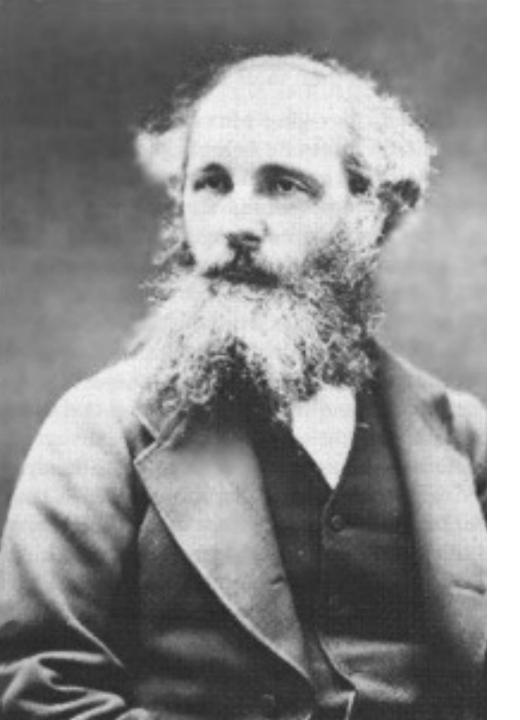






Michael Faraday





Founder of electromagnetism

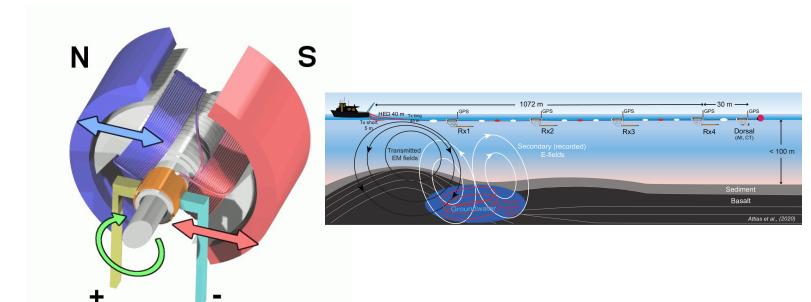
James Clerk Maxwell: (1839-1879)
Scottish mathematician

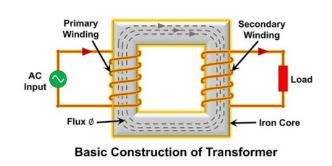
- Developed a scientific theory to explain electromagnetic fields and waves
- Coupled the electrical fields and magnetic fields together
- Established the foundations of electricity and magnetism as electromagnetism
- Maxwell's equations

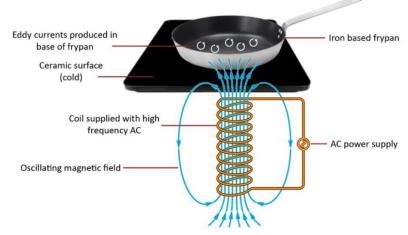
Daily life applications

For example:

- Electric motor/generator
- Water/minerals exploration
- Transformer
- Induction oven
- •

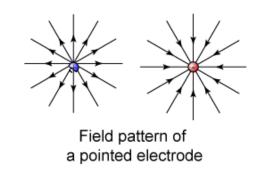


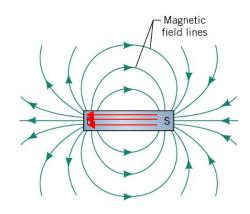




Electromagnetism: Maxwell's equations

- A static electric charges produces an electric field
- There is no magnetic charge (monopole)
- A changing magnetic field produces an electric field
- Charges in motion (an electrical current) produce a magnetic field
- A changing electric field produces a magnetic field





Electric and magnetic fields can produce forces on charges

$$\nabla \cdot \mathbf{E} = \frac{\rho}{\epsilon_0},$$

$$\nabla \cdot \mathbf{B} = 0,$$

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t},$$

$$\frac{1}{u_0} \nabla \times \mathbf{B} = \epsilon_0 \frac{\partial \mathbf{E}}{\partial t} + \mathbf{J}.$$

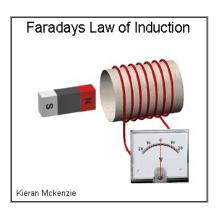
E: electric field, vector

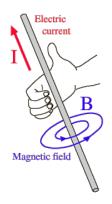
D: electric flux density, vector

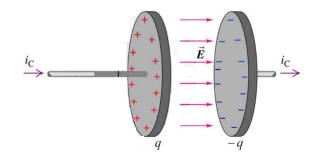
H: magnetic field, vector

B: magnetic flux density, vector

J: current density, vector ρ: static charge density



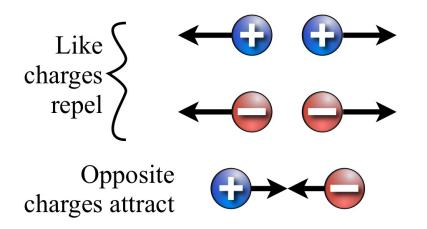




Electricity and magnetism had been unified into electromagnetism!

Coulomb's law: force between electrostatic charges

Published in 1785 by French physicist <u>Charles-Augustin de Coulomb</u> and was essential to the development of the <u>theory of electromagnetism</u>



Scalar:
$$F = k \frac{q_1 q_2}{r_{12}^2} = \frac{q_1 q_2}{4\pi \epsilon_0 r_{12}^2}$$

Vector:
$$\overrightarrow{F} = \frac{q_1q_2}{4\pi\varepsilon_0r_{12}^2}\widehat{r_{12}}$$

 $\widehat{r_{12}}$ is for direction, its absolute value is 1

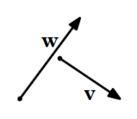
 $k = 9 \times 10^9 \text{Nm}^2/\text{C}^2$, Coulomb's constant

The electrostatic force had the same functional form as Newton's law of gravity The magnitude of the electrostatic force between two-point charges:

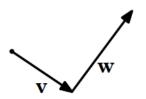
- 1) Directly proportional to the product of the magnitudes of charges
- 2) Inversely proportional to the square of the distance between them
- 3) The force is along the straight line joining them

Vector calculus:

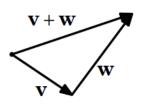




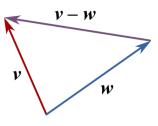




(b) Translate w to the end of v

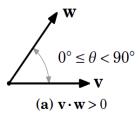


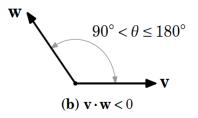
(c) The sum $\mathbf{v} + \mathbf{w}$

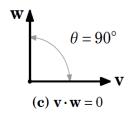


Dot product

$$\mathbf{v} \cdot \mathbf{w} = \cos \theta \| \mathbf{v} \| \| \mathbf{w} \|$$





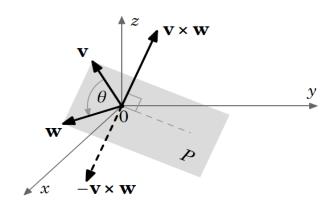


$$V = (1, 0)$$

 $W = (0, 1)$

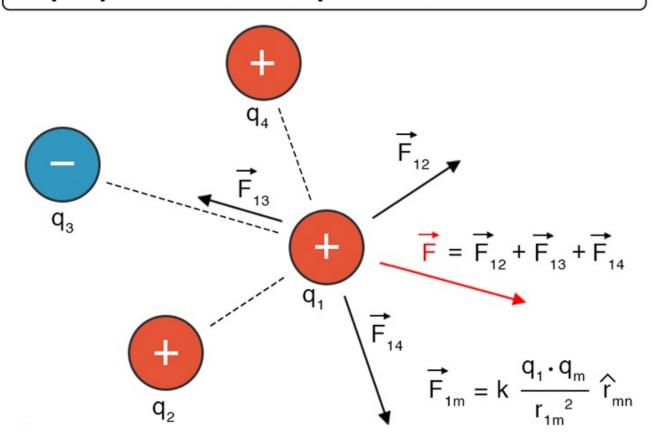
Cross product

$$\|\mathbf{v} \times \mathbf{w}\| = \|\mathbf{v}\| \|\mathbf{w}\| \sin \theta$$



Vector force

Superposition Principle of Coulomb's Law



$$\vec{F}_{tot} = \sum_{i=1}^{n} \frac{qq_i}{4\pi\varepsilon_0 r_i^2} \hat{r}_i$$

$$\overrightarrow{F}_{tot} = \sum_{i=2}^{4} \frac{q_1 q_i}{4\pi \varepsilon_0 r_i^2} \widehat{r}_i$$

Line integral of vector

Line integral of vector force **F** along the curve **C**.

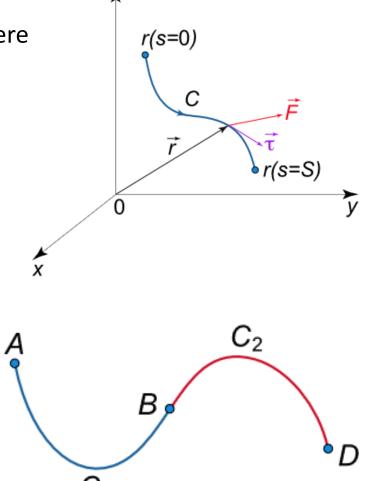
Suppose that a curve \mathbf{C} is defined by the vector function r=r(s), $0 \le s \le S$, where s is the arc length of the curve. Then the derivative of the vector function

$$\frac{d\mathbf{r}}{ds} = \boldsymbol{\tau}$$
 (Tangent direction at each point of the curve)

Curve direction is important.

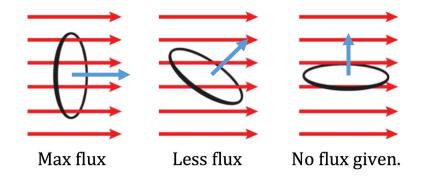
$$\int\limits_{C}\left(\mathbf{F}\cdot d\mathbf{r}
ight)=\int\limits_{0}^{S}\left(\mathbf{F}\left(\mathbf{r}\left(s
ight)
ight)\cdotoldsymbol{ au}
ight)ds,$$

$$\int\limits_C \left(\mathbf{F} \cdot d\mathbf{r}
ight) = \int\limits_{C_1 \cup C_2} \left(\mathbf{F} \cdot d\mathbf{r}
ight) = \int\limits_{C_1} \left(\mathbf{F} \cdot d\mathbf{r}
ight) + \int\limits_{C_2} \left(\mathbf{F} \cdot d\mathbf{r}
ight);$$

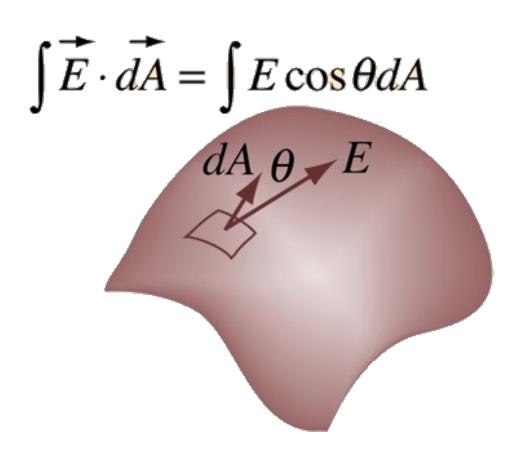


Surface integral of vector

dA direction is <u>perpendicular</u> to the <u>tangent plane</u> to that surface at A



$$\iint_{S} \mathbf{E} \cdot d\mathbf{A} = \iint_{S} \mathbf{E} \cdot \hat{\mathbf{n}} dA$$



Gradient

Gradient: 3-dimension derivative of a scalar function

Showing the **direction and rate of of fastest increase** of the scalar function f at a point space

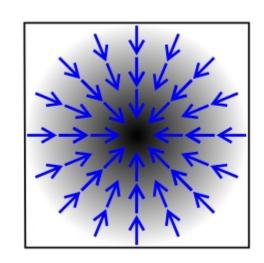
How quickly something changes from one point to another

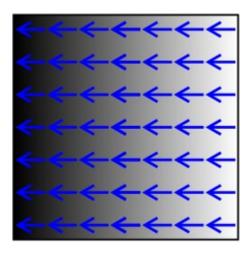
$$\nabla f = \frac{\partial f}{\partial x} \widehat{x} + \frac{\partial f}{\partial y} \widehat{y} + \frac{\partial f}{\partial z} \widehat{z}$$

f: Scalar function

 ∇f (Gradient): Vector function

Direction: Rate of the fastest increase



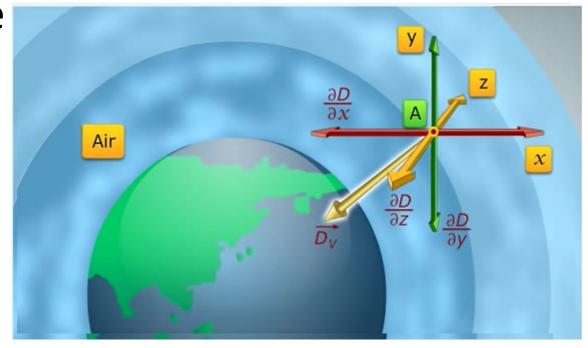


Example: air density in the space

$$D = f(x, y, z)$$

$$\nabla = \frac{\partial}{\partial x} \widehat{\boldsymbol{x}} + \frac{\partial}{\partial y} \widehat{\boldsymbol{y}} + \frac{\partial}{\partial z} \widehat{\boldsymbol{z}}$$

$$\nabla D = \frac{\partial D}{\partial x} \widehat{\boldsymbol{x}} + \frac{\partial D}{\partial y} \widehat{\boldsymbol{y}} + \frac{\partial D}{\partial z} \widehat{\boldsymbol{z}}$$



Maximum rate at which the Density Increases

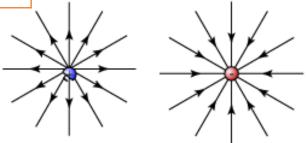
Divergence: Flux/field out of a point

Divergence represents the volume density of the outward <u>flux</u> of a vector field from an infinitesimal volume around a given point

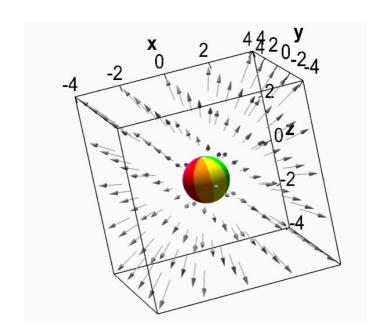
$$\operatorname{div}\mathbf{F}|_{\mathbf{x_0}} = \lim_{V o 0} rac{1}{|V|} \iint_{S(V)} \mathbf{F} \cdot \hat{\mathbf{n}} \, dS$$

$$\operatorname{div}\mathbf{F} = \mathbf{\nabla} \cdot \mathbf{F} = \frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y} + \frac{\partial F_z}{\partial z}$$

F is a vector **∇** · **F** is a scalar



Field pattern of a pointed electrode

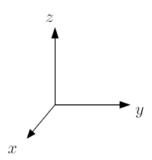


Divergence: mathematical calculation

$$\operatorname{div} \mathbf{A} = \lim_{\Delta v \to 0} \frac{\oint_S \mathbf{A} \cdot d\mathbf{S}}{\Delta v}.$$

$$\oint_{S} \mathbf{A} \cdot d\mathbf{S} = \oint_{S} \mathbf{A} \cdot \hat{\mathbf{n}} dS$$

dydz is total area



$$\mathbf{A} = (A_x, A_y, A_z)$$

$$dz$$

$$P$$

$$dy$$

$$P = (x_0, y_0, z_0)$$

$$\oint_{S} \mathbf{A} \cdot d\mathbf{S} = \int_{\text{foran}} A_{x}(\text{foran}) dy dz - \int_{\text{bak}} A_{x}(\text{bak}) dy dz \qquad A_{x}(\text{foran}) - A_{x}(\text{bak}) = A_{x}(x_{0} + dx/2, y_{0}, z_{0}) - A_{x}(x_{0} - dx/2, y_{0}, z_{0}) = \frac{\partial A_{x}}{\partial x} dx \\
- \int_{\text{venstre}} A_{y}(\text{venstre}) dx dz + \int_{\text{høyre}} A_{y}(\text{høyre}) dx dz \qquad A_{y}(\text{høyre}) - A_{y}(\text{venstre}) = \frac{\partial A_{y}}{\partial y} dy \\
+ \int_{\text{topp}} A_{z}(\text{topp}) dx dy - \int_{\text{bunn}} A_{z}(\text{bunn}) dx dy. \qquad A_{z}(\text{topp}) - A_{z}(\text{bunn}) = \frac{\partial A_{z}}{\partial z} dz.$$

$$\oint_{S} \mathbf{A} \cdot d\mathbf{S} = \frac{\partial A_{x}}{\partial x} dx dy dz + \frac{\partial A_{y}}{\partial y} dx dy dz + \frac{\partial A_{z}}{\partial z} dx dy dz$$

$$\operatorname{div} \mathbf{A} = \lim_{\Delta v \to 0} \frac{\oint_{S} \mathbf{A} \cdot d\mathbf{S}}{\Delta v}.$$

 $\Delta v = \mathrm{d}x\mathrm{d}y\mathrm{d}z$

$$\operatorname{div} \mathbf{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} = \nabla \cdot \mathbf{A}.$$

Divergence theorem

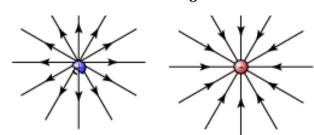
It states that the surface integral of a vector field over a closed surface is equal to the volume integral of the divergence over the region inside the surface.

$$\oint_{S} \mathbf{A} \cdot d\mathbf{S} = \int_{v} \nabla \cdot \mathbf{A} dv$$

$$\oint_{S} \mathbf{E} \cdot d\mathbf{S} = \sum_{i} \oint_{S_{i}} \mathbf{E} \cdot d\mathbf{S} = \sum_{i} \left(\frac{1}{\Delta V_{i}} \oint_{S_{i}} \mathbf{E} \cdot d\mathbf{S}_{i}\right) \Delta V_{i} \to \int \nabla \cdot \mathbf{E} dV_{i}$$

$$abla \cdot E = rac{
ho}{arepsilon_0}$$
 Gauss

Gauss's Law



en del av S

Field pattern of a pointed electrode

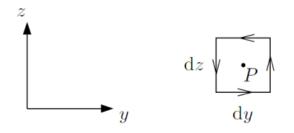
Curl

The curl of a field presents the infinitesimal circulation density at each point of the field

How much does a field circulate around a point

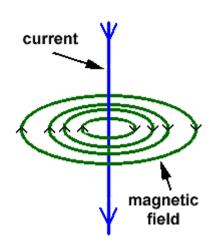
One dimension x

$$(\operatorname{curl} \mathbf{A})_x = \lim_{\Delta S \to 0} \frac{\oint_C \mathbf{A} \cdot \mathrm{d}\mathbf{l}}{\Delta S}$$



Three dimensions x, y and z

$$\nabla \times \mathbf{A} = \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z}\right) \hat{\mathbf{x}} + \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x}\right) \hat{\mathbf{y}} + \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y}\right) \hat{\mathbf{z}}$$



Curl

The curl around x-axis, in yz plane

$$\oint_{C} \mathbf{A} \cdot d\mathbf{l} = \int_{\text{nede}} A_{y}(\text{nede}) dy - \int_{\text{oppe}} A_{y}(\text{oppe}) dy - \int_{\text{venstre}} A_{z}(\text{venstre}) dz + \int_{\text{høyre}} A_{z}(\text{høyre}) dz$$

$$A_y(\text{nede}) - A_y(\text{oppe}) = A_y(x_0, y_0, z_0 - dz/2) - A_y(x_0, y_0, z_0 + dz/2) = -\frac{\partial A_y}{\partial z} dz,$$

$$A_z(\text{høyre}) - A_z(\text{venstre}) = A_z(x_0, y_0 + dy/2, z_0) - A_z(x_0, y_0 - dy/2, z_0) = \frac{\partial A_z}{\partial y} dy,$$

$$\oint_C \mathbf{A} \cdot d\mathbf{l} = \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z}\right) dy dz,$$

$$(\operatorname{curl} \mathbf{A})_x = \frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z}.$$

Similar to the curl around y and z-axis

$$\nabla \times \mathbf{A} = \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z}\right) \widehat{\mathbf{x}} + \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x}\right) \widehat{\mathbf{y}} + \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y}\right) \widehat{\mathbf{z}}$$

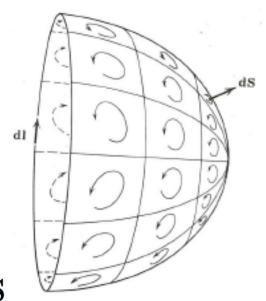
Stokes' theorem

Given a vector field, the theorem relates the integral of the curl of the vector field over a surface, to the line integral of the vector field around the boundary of the surface.

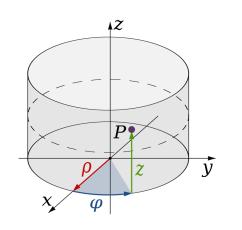
$$\oint_C \mathbf{A} \cdot d\mathbf{l} = \int_S \nabla \times \mathbf{A} \cdot d\mathbf{S}.$$

$$\int_{S} \nabla \times \mathbf{A} \cdot d\mathbf{S} = \sum_{i} \oint_{C_{i}} \mathbf{A} \cdot d\mathbf{l}.$$

$$\oint_{C} \mathbf{E} \cdot d\mathbf{l} = \sum_{i} \oint_{C_{i}} \mathbf{E} \cdot d\mathbf{l} = \sum_{i} \left(\frac{\oint_{S_{i}} \mathbf{E} \cdot d\mathbf{S}_{i}}{\Delta S_{i}} \right) \Delta S_{i} \to \int \nabla \times \mathbf{E} \cdot d\mathbf{S}$$

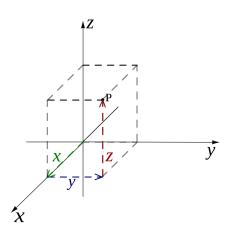


Different coordinates



Cylindrical coordinate

$$egin{aligned} x &=
ho\cosarphi \ y &=
ho\sinarphi \ z &= z \end{aligned}$$



Cartesian Coordinate

$$\nabla = \frac{\partial}{\partial x} \widehat{\boldsymbol{x}} + \frac{\partial}{\partial y} \widehat{\boldsymbol{y}} + \frac{\partial}{\partial z} \widehat{\boldsymbol{z}}$$

$$\nabla D = \frac{\partial D}{\partial x} \hat{\boldsymbol{x}} + \frac{\partial D}{\partial y} \hat{\boldsymbol{y}} + \frac{\partial D}{\partial z} \hat{\boldsymbol{z}}$$

$$\nabla \cdot \mathbf{F} = \frac{\partial F_{x}}{\partial x} + \frac{\partial F_{y}}{\partial y} + \frac{\partial F_{z}}{\partial z}$$

$$abla f = rac{\partial f}{\partial
ho} oldsymbol{\hat{
ho}} + rac{1}{
ho} rac{\partial f}{\partial arphi} oldsymbol{\hat{arphi}} + rac{\partial f}{\partial z} oldsymbol{\hat{z}}$$

$$abla \cdot oldsymbol{A} = rac{1}{
ho} rac{\partial}{\partial
ho} \left(
ho A_
ho
ight) + rac{1}{
ho} rac{\partial A_arphi}{\partial arphi} + rac{\partial A_z}{\partial z}$$

$$\nabla \times \mathbf{A} = \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z}\right) \hat{\mathbf{x}} + \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x}\right) \hat{\mathbf{y}} + \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y}\right) \hat{\mathbf{z}}$$

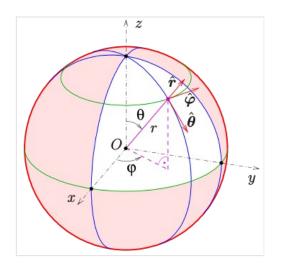
$$abla imes oldsymbol{A} = \left(rac{1}{
ho}rac{\partial A_z}{\partial arphi} - rac{\partial A_arphi}{\partial z}
ight) oldsymbol{\hat{
ho}} + \left(rac{\partial A_
ho}{\partial z} - rac{\partial A_z}{\partial
ho}
ight) oldsymbol{\hat{arphi}} + rac{1}{
ho}\left(rac{\partial}{\partial
ho}\left(
ho A_arphi
ight) - rac{\partial A_
ho}{\partial arphi}
ight) oldsymbol{\hat{z}}$$

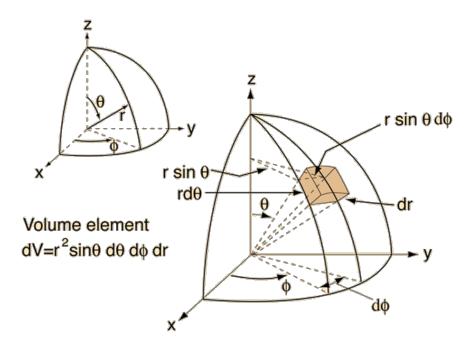
Different coordinates

 $x = r \sin \theta \cos \varphi$,

 $y = r \sin \theta \sin \varphi$,

 $z = r \cos \theta$.





$$abla f = rac{\partial f}{\partial r}\hat{\mathbf{r}} + rac{1}{r}rac{\partial f}{\partial heta}\hat{oldsymbol{ heta}} + rac{1}{r\sin heta}rac{\partial f}{\partial arphi}\hat{oldsymbol{arphi}},$$

$$abla \cdot \mathbf{A} = rac{1}{r^2} rac{\partial}{\partial r} \left(r^2 A_r
ight) + rac{1}{r \sin heta} rac{\partial}{\partial heta} \left(\sin heta A_ heta
ight) + rac{1}{r \sin heta} rac{\partial A_arphi}{\partial arphi},$$

$$egin{align}
abla imes \mathbf{A} &= rac{1}{r \sin heta} \left(rac{\partial}{\partial heta} \left(A_{arphi} \sin heta
ight) - rac{\partial A_{ heta}}{\partial arphi}
ight) \hat{\mathbf{r}} \ &+ rac{1}{r} \left(rac{1}{\sin heta} rac{\partial A_r}{\partial arphi} - rac{\partial}{\partial r} \left(r A_{arphi}
ight)
ight) \hat{oldsymbol{ heta}} \end{aligned}$$

$$+ \, rac{1}{r} \left(rac{\partial}{\partial r} \left(r A_{ heta}
ight) - rac{\partial A_r}{\partial heta}
ight) \hat{oldsymbol{arphi}},$$

$$x^2 + y^2 + z^2 = a^2 \qquad \Longrightarrow \qquad r = a$$

Example 1:

Calculate the integral

$$I = \int_{V} (\nabla \cdot \mathbf{F}) dV \tag{1}$$

where $\mathbf{F} = r\hat{\mathbf{r}} = x\hat{\mathbf{x}} + y\hat{\mathbf{y}} + z\hat{\mathbf{z}}$, and the volume V is a sphere with radius R placed in the origin.

- a) Calculate the integral directly.
- b) Calculate the integral using the divergence theorem.

$$\operatorname{div} \mathbf{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} = \nabla \cdot \mathbf{A}.$$

$$\oint_{S} \mathbf{A} \cdot d\mathbf{S} = \int_{v} \nabla \cdot \mathbf{A} dv$$

Solution for a

Calculate the integral

$$I = \int_{V} (\nabla \cdot \mathbf{F}) dV \tag{1}$$

where $\mathbf{F} = r\hat{\mathbf{r}} = x\hat{\mathbf{x}} + y\hat{\mathbf{y}} + z\hat{\mathbf{z}}$, and the volume V is a sphere with radius R placed in the origin.

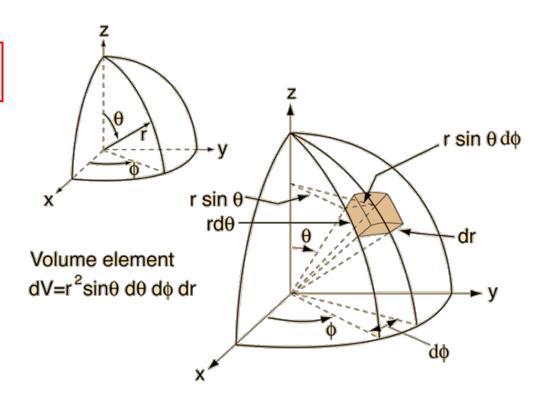
- a) Calculate the integral directly.
- b) Calculate the integral using the divergence theorem.

$$\nabla \cdot \mathbf{F} = 3.$$

$$\operatorname{div} \mathbf{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} = \nabla \cdot \mathbf{A}.$$

$$\int_{v} (\nabla \cdot \mathbf{F}) dV = \int_{0}^{R} \int_{0}^{2\pi} \int_{0}^{\pi} 3r^{2} \sin \theta d\varphi d\theta dr$$
$$= 3 \int_{0}^{R} r^{2} dr \int_{0}^{\pi} \sin \theta d\theta \int_{0}^{2\pi} d\varphi$$
$$= \underline{4\pi R^{3}}.$$

$$\int_{V} (\nabla \cdot \mathbf{F}) dV = 3 \int_{V} dV = 4\pi R^{3}.$$



Solution for b

$$\mathbf{F} = r\mathbf{\hat{r}} = x\mathbf{\hat{x}} + y\mathbf{\hat{y}} + z\mathbf{\hat{z}}$$

$$\oint_{S} \mathbf{A} \cdot d\mathbf{S} = \int_{v} \nabla \cdot \mathbf{A} dv$$

$$\int_{v} (\nabla \cdot \mathbf{F}) dv = \oint_{S} \mathbf{F} \cdot d\mathbf{S}$$

$$= \int_{0}^{2\pi} \int_{0}^{\pi} (R\hat{\mathbf{r}}) \cdot (R^{2} \sin \theta d\theta d\varphi \hat{\mathbf{r}})$$

$$= R^{3} \int_{0}^{2\pi} d\varphi \int_{0}^{\pi} \sin \theta d\theta$$

$$= \underline{4\pi R^{3}}.$$

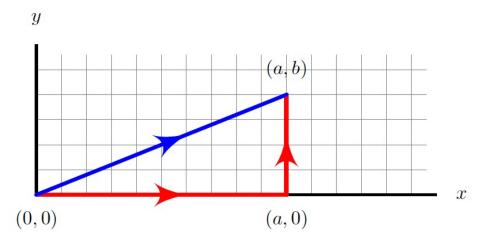
Example 2:

Calculate the line integral

$$I = \int_C \mathbf{F} \cdot d\mathbf{l},\tag{2}$$

Where $\mathbf{F} = (xy^2 + 2y)\hat{\mathbf{x}} + (x^2y + 2x)\hat{\mathbf{y}}$,

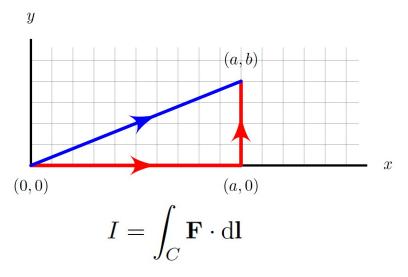
- i) Along the curve C_1 which consists of two straight lines connecting the points (0,0), (a,0) and (a,b), see figure below.
- ii) Along the curve C_2 which consists of one straight line connecting the points (0,0) and (a,b), see figure below.
- iii) Why do these calculations produce the same answer? Explain using Stoke's theorem.



$$\oint_C \mathbf{A} \cdot d\mathbf{l} = \int_S \nabla \times \mathbf{A} \cdot d\mathbf{S}.$$

$$\nabla \times A = \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z}\right) \hat{x} + \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x}\right) \hat{y} + \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y}\right) \hat{z}$$

Solution for i) and ii)



$$\mathbf{F} = (xy^2 + 2y)\hat{\mathbf{x}} + (x^2y + 2x)\hat{\mathbf{y}}$$
$$d\mathbf{l} = dx\hat{\mathbf{x}} + dy\hat{\mathbf{y}}.$$

$$\mathbf{F} \cdot d\mathbf{l} = F_x dx + F_y dy$$
$$= (xy^2 + 2y)dx + (x^2y + 2x)dy.$$
$$y = \frac{bx}{a}$$

i) Along the curve C_1 which consists of two straight lines connecting the points (0,0), (a,0) and (a,b), see figure below.

$$I = \int_C \mathbf{F} \cdot d\mathbf{l}$$
$$= \int_0^b (a^2y + 2a)dy$$
$$= \frac{1}{2}a^2b^2 + 2ab.$$

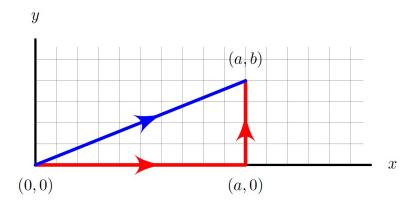
ii) Along the curve C_2 which consists of one straight line connecting the points (0,0) and (a,b), see figure below.

$$I = \int_{C} \mathbf{F} \cdot d\mathbf{l}$$

$$= \int_{0}^{a} \left[x \left(\frac{bx}{a} \right)^{2} + 2 \left(\frac{bx}{a} \right) \right] dx + \int_{0}^{b} \left[\left(\frac{ay}{b} \right)^{2} y + 2 \left(\frac{ay}{b} \right) \right] dy$$

$$= \underbrace{\frac{1}{2} a^{2} b^{2} + 2ab}.$$

Solution for iii)



$$\nabla \times \mathbf{A} = \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z}\right) \hat{\mathbf{x}} + \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x}\right) \hat{\mathbf{y}} + \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y}\right) \hat{\mathbf{z}}$$

iii) Why do these calculations produce the same answer? Explain using Stoke's theorem.

$$\mathbf{F} = (xy^2 + 2y)\mathbf{\hat{x}} + (x^2y + 2x)\mathbf{\hat{y}}$$

These integrals have equal values since \mathbf{F} is a conservative field:

$$\oint_C \mathbf{A} \cdot d\mathbf{l} = \int_S \nabla \times \mathbf{A} \cdot d\mathbf{S}.$$

$$\nabla \times \mathbf{F} = \left(\frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y}\right) \hat{\mathbf{z}}$$
$$= (2xy - 2xy) \hat{\mathbf{z}}$$
$$= 0.$$